











Computer Aided Battery Engineering Consortium



P.I.: Almad Pesaran

NRÉL Contributors: Shriram Santhanagopalan, Kandler Smith, Lei Cao, Gi-Heon Kim, Chao Zhang, Chuanbo Yang, Peter Graf Partner Contributors: Stephen Dajka (ANSYS), Partha Mukherjee (TAMU) Elham Sahraei (MIT), Josh Lamb (SNL), Dennis Dees (ANL) Bill Stanko (USCAR)

National Renewable Energy Laboratory
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Project ID # ES294

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Overview – A New Project for FY16

Timeline

Project Start Date: 10/2015

Project End Date: 9/2018

Percent Complete: 17%

Budget

- Total Project Funding: \$1.735M
 - DOE Share: 100%
 - Contractor Share: 0%
- Funding Received in FY16: \$1.735M
- Subcontractors Funding: \$400K

Barriers

- Lack of tools that can simulate battery thermal behavior during crush for improving battery safety
- Lack of fast CAEBAT software
- Lack of microstructure models for electrode design

Partners

- ANSYS
- ANL
- SNL
- MIT
- Texas AMU
- USCAR-CSWG









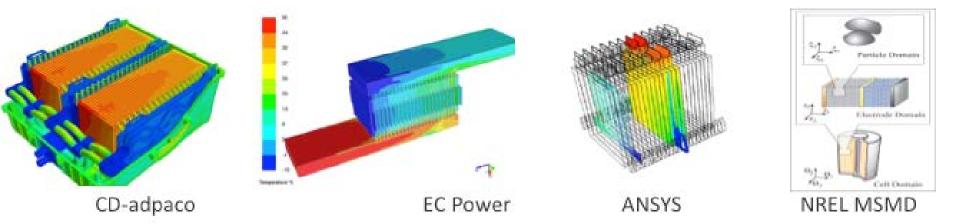






Relevance – Supporting DOE VTO Program

- The DOE's EV Everywhere Grand Challenge aims to produce plug-in electric vehicles (PEVs) as affordable, safe, and convenient for the American family as gasoline-powered vehicles by 2022.
 - PEVs must be as safe as conventional vehicles.
 - PEV batteries must not lead to unsafe situations when crashed
- The 2011–2014 DOE VTO Computer Aided Engineering for Electric Drive Vehicle (CAEBAT) activity was successful in releasing electrochemical-thermal models in commercial software tools.









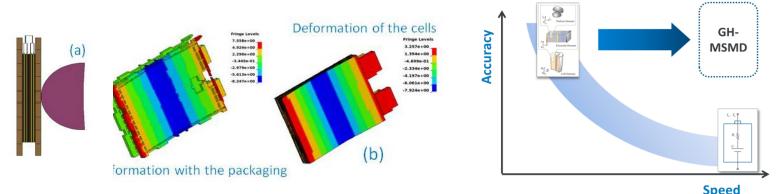






Relevance – Supporting VTO CAEBAT Activity

- FY13-FY14 NREL projects funded under FY13 DOE VTO FOA (dubbed as CAEBAT-II) initiated the following:
 - 1. Linking <u>mechanical</u> models to <u>electrochemical-thermal</u> tools to study crash-induced crush and
 - 2. Speeding up the computational time of running simulations



- This FY16 project is based on a proposal awarded under the FY15
 VTO FOA (CAEBAT-II) and has started in October 2015.
- The overall goal of all CAEBAT phases is to create CAE tools to reduce the development cycle of safe in-vehicle battery systems, thus reducing costs of batteries and making PEVs affordable.

Relevance – Project Objectives

Purpose: Assemble a multi-national lab collaborative team including experts from academia and industry to enhance recently developed CAEBAT-II battery crush modeling tools and to develop microstructure models for electrode design – both computationally efficient

The objectives are to:

- 1. Enhance extremely fast multi-physics battery models
- Couple mechanical-electro-chemical-thermal (MECT) models more efficiently
- 3. Develop advanced microstructure models for Li-ion electrodes













Key Milestones – by Tasks

Milestone Name/Description	Deadline	Milestone Type
M 1.1 Draft Summary Documentation of GH-MSMD framework	09/31/2016	Annual SMART Milestone
M 1.2 Complete Frequency Domain GH-MSMD formulation	01/31/2017	Quarterly Progress Measure
M 1.3 Present at the DOE Annual Merit Review	04/30/2016	Quarterly Progress Measure
M 1.4 Perform out design evaluation and performance evolution study using newly developed multiphysics GH-constituent models	07/31/2018	Quarterly Progress Measure
M 2.1 Present initial demonstration of simultaneous coupling in MECT model that shows interaction of mechanical deformation with the thermal response	03/31/2016	Milestone (Go/No-Go)
M 2.2 Draft documentation describing the mechanical tests procedure for development and validation of constitutive models for individual battery components	07/31/2017	Annual SMART Milestone
M 2.3 Interim update on mechanical models demonstrating damage propagation across multiple axes of battery cells and battery modules	12/31/2017	Quarterly Progress Measure
M 2.4 Report summarizing model validation for MECT simulations	04/30/2018	Quarterly Progress Measure
M.3.1 Document microstructure model formulation and validation plan	12/31/2015	Quarterly Progress Measure
M 3.2 Present microstructure project update at AMR	06/31/2016	Quarterly Progress Measure
M 3.3 Comparison of microstructural model simulations from both stochastic reconstructed (simulated) and tomographic (measured) geometries	09/30/2017	Quarterly Progress Measure (Go/No-Go)
M 3.4Validation of electrode microstructure design tool for multiple electrode designs showing < 10% error between models and data	09/30/2018	Annual SMART Milestone

FY16 Project Milestones

Milestone Name/Description	Due Date	Milestone Type	Status
Develop microstructure model formulation and validation plan	12/31/2015	QPM (Regular)	Complet
Present initial demonstration of simultaneous coupling approach for connecting mechanical deformations to electro-chemical-thermal models	3/31/2016	Go-No Go QPM (Stretch)	Completed
Attend the DOE Annual Merit Review to update on project progress	6/30/2016	QPM (Regular)	On Track
Draft Summary Documentation of GH- MSMD framework	9/31/2016	Annual SMART (Regular)	On Track

QPM: Quarterly Progress Measure















Strategy/Approach – End Goals

- Expand upon existing electro-chemical-thermal (ETC) and mechanical-ETC models, make them computationally more efficient, add new physics, develop microstructure models, validate them
- Accelerate developing improved electrode and cells by reducing the number of experiments
- Transfer developed models to commercial software vendors and end-users to reduce the battery development cycle and cost.













Strategy/Approach - Tasks

- 1. Enhance extremely fast multiphysics battery models for particle, electrode-, cell-, and pack-level multiscale model simulations based on the innovative GH-MSMD developed under CAEBAT-2. Fabricate and test electrode and cells for model parameter identification and validation.
- 2. Couple mechanical-electro-chemical-thermal (MECT) models efficiently to predict the thermal-runaway behavior of cells and modules after a crash-induced crush, expanding on the unique approach developed in CAEBAT-2. Perform battery abuse and safety testing for parameterization and validation of models. Obtain insight from automotive crash experts.
- 3. Develop advanced microstructure models as tools to design battery electrodes through a better understanding of basic physics at the particle and electrode levels. Build upon exiting microstructure models. Fabricate and test electrode samples with different characteristics, also obtain tomography images, to build enhanced and validated microstructure models.

Strategy/Approach: Roles-Responsibility

- NREL (Gi-Heon Kim) leads Task 1. Enhancing extremely fast multiphysics battery models,
 - ANL fabricates electrode and cells samples and conduct experiments.
 - NREL enhances fast-running MSMD framework to include new physics
- NREL (Shriram Santhanagopalan) leads Task 2. Coupled Mechanical ETC modeling
 - MIT performs experiments for mechanical properties
 - ANL fabricates appropriate cells
 - SNL conducts abuse test (crush & circuit)
 - NREL furthers enhance MECT models for cells and modules
 - NREL compare SNL data with models for validation
 - CSWG provide insight battery crush testing and industry perspective
 - The ANSYS team will participate in integrating the MECT models with Fluent and commercializing the solution.

Strategy/Approach: Roles-Responsibilities

- NREL (Kandler Smith) leads Task 3. Developing Advanced microstructure models task
 - ANL fabricates electrodes and map microstructure geometry using tomographic imaging
 - ANL conducts experiments on electrode with different characteristics
 - TAMU creates microstructure geometry and link to electrochemical models
 - NREL integrates the microstructure models into the CAEBAT framework
 - NREL/TAMU use the experimental data for validation and further enhancement
- Ahmad Pesaran (NRE) leads the overall project









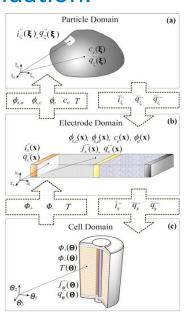






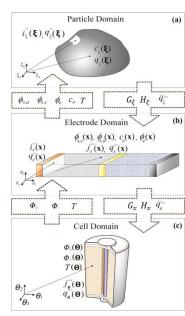
Technical Accomplishments – Task 1

1. Enhancing extremely fast multiphysics battery models for particle, electrode-, cell-, and pack-level multiscale model simulations based on the innovative GH-MSMD developed under CAEBAT-2. Fabricate and test electrode and cells for model parameter identification and validation.



MSMD

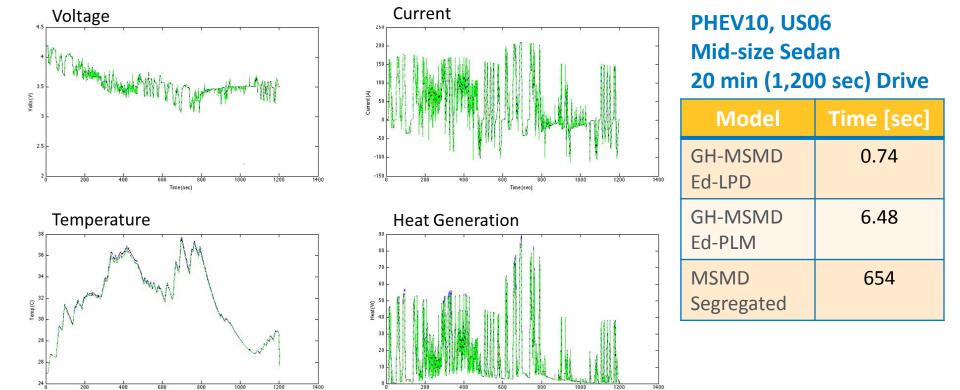
MSMD vs GH-MSMD



GH-MSMD

The diagrams above summarize the model solution variables in each computational domain and the coupling variables exchanged between the adjacent length scale domains in MSMD (left) and in GH-MSMD (right). Even though the solution algorithms are significantly different between the two, the model structures are similar. This comparison signifies the modularity of model framework that the GH-MSMD inherited from the MSMD.

Benchmark Result of GH-MSMD Implementation



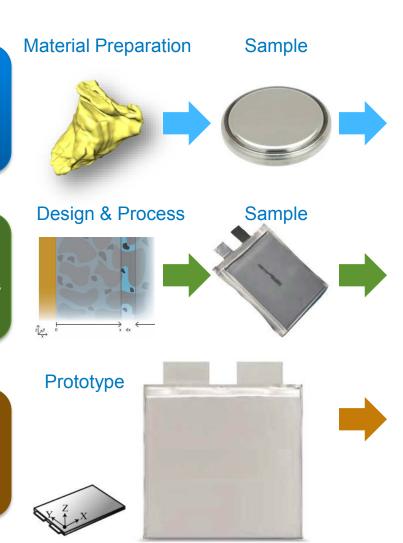
Figures above present the comparison of electrical and thermal response of a battery for mid-size sedan plug-in hybrid electric vehicle (PHEV10) US06 20 minutes driving power profile from the GH-MSMD and the original MSMD. The model outputs are shown very close to each other. The most efficient GH-MSMD model option runs the 1,200-second simulation only in 0.74 seconds using a personal computer, while the original MSMD runs the same case in 654 seconds.

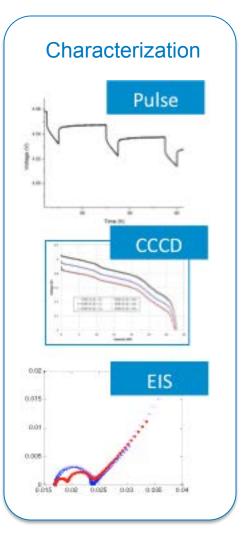
- A 100~1,000 fold speed up was demonstrated while maintaining solution accuracy.
- Submitted a manuscript (titled *Efficient and Extensible Quasi-Explicit Modular Nonlinear Multiscale Battery Model: GH-MSMD*) to Journal of Power Sources
- Continued development of standard procedure for MSMD/GH-MSMD model parameter identification

Model Parameter Identification

Intrinsically Under-determined Problem

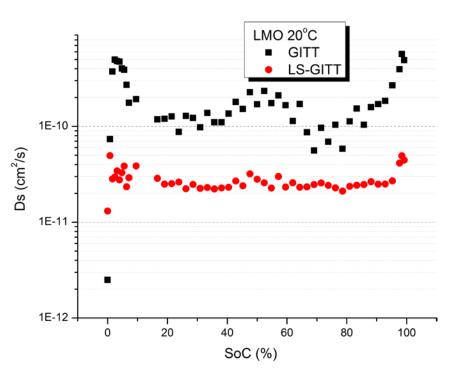
- Thermodynamic properties
- Kinetics characteristics
- Ion transport characteristics
- Electrical characteristics
- Particle geometry/morphology
- Pore structure characteristics
- Transport limitation in electrolyte
- Ionic conductance
- Electronic conductance in matrices
- N-P balance
- Functional additive effects
- Thermal mass and conductance
- Electrode terminals and current collectors
- Performance evaluation
- Safety evaluation
- Life evaluation





Challenges: Inconsistency

Diffusivity: GITT vs LS-GITT



It is shown that two conventional methods (using different models) yield different diffusivity values from an identical experimental data set.

- Physics-based models are constructed on governing equations describing physicochemical processes in a battery, and require related material properties and design parameters as model inputs.
- On the other hand, standard characterization tests such as GITT and EIS use certain models while acquiring physicochemical properties of battery components.
- Unfortunately, these procedures have been decoupled in practice.

[APPROCH] Advanced Model-based Battery System Characterization

- Model-based optimization procedures that have been highly desired by battery industry, but limited by the lack of a fully-adaptive, fastrunning, high-fidelity, flexible battery model.
- NREL brings high fidelity fast-running models directly into battery system characterization step.

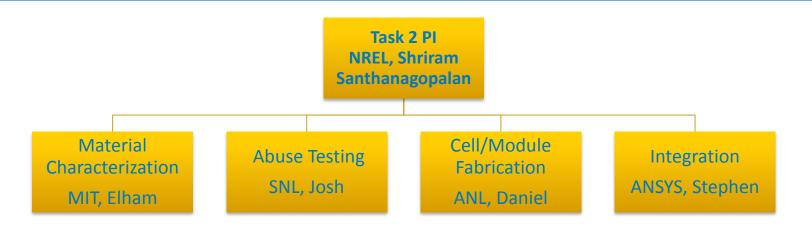
Approaches : 5 Sub-Tasks

- 1.1. *Enhance Baseline Model Capabilities*: GH-baseline models were successfully developed and implemented both in Matlab and C++ platform. We found that major enhancement of these models are required for better use in application for advanced model-based battery characterization. This subtask includes improving PDM particle network model and enhancing CDM sparse-matrix treatment.
- 1.2. **Develop Frequency Domain GH-MSMD Framework**: EIS is one of the frequently used experimental methods for battery characterization and diagnostics. Since the current GH-MSMD has been developed in time-domain, it is difficult to utilize the information produced in frequency domain. In this subtask, frequency-domain GH-MSMD will be developed from the governing equations used in time-domain model, running with the identical model input files.
- 1.3. *Develop Physics-based Constituent Models for Design Evaluation and Performance Evolution*: The purely predictive models will only require material characteristics, design parameters, and process parameters to predict the performance and the life of a battery before it is actually made. To meet the eventual goal providing such models, we will develop proper GH-constituent models capturing physicochemical processes.

Future Work for Task 1

- Enhance Baseline Model Capabilities
- Develop Frequency Domain GH-MSMD Framework
- Develop Physics-based Constituent Models for Design Evaluation and Performance Evolution
- GH-MSMD Documentation for Battery Community
- Fabrication and Characterization

Task 2 – Mechanical –ECT Coupling



- The main objective of this effort is to develop a physically accurate mechanicalelectrochemical-thermal modeling approach to simulate the interplay of mechanical crush with thermal and electrochemical responses of the battery under various abuse scenario.
- To accomplish this, we will expand the unique approach developed in CAEBAT-2 to enable simultaneously coupling of mechanical-electrochemical-thermal behaviors, and accurate modeling of mechanical failure events.
- We will build cell-level models for a subsequent milestone and are collaborating with MIT and SNL to obtain test data to characterize the model parameters as well as to validate cell-level predictions from these models.

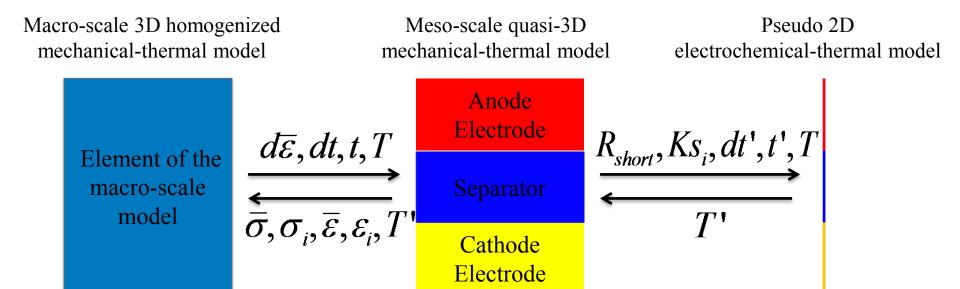
Technical Accomplishment - Task 2

- Developed a material model for simultaneously modeling of mechanicalelectrochemical-thermal behavior
- Predicted the electrical short, voltage drop and thermal runaway behaviors followed by a mechanical abuse induced short
- Studied the effect of short resistance on the battery cell performance
- Demonstrating the applicability of the developed model for full pouch cell abuse simulation
- Received first round of data from SNL on abuse test of battery module
- Implementing ABDT tool into standard ANSYS System in Workbench

Milestone: Identify an Approach to Simultaneously Link Crush Simulations to ECT

 This Milestone was completed in March 2016 showing some initial results on a model geometry. The results indicate a "Go" on this milestone.

NREL Multi-scale Simultaneously Coupled MECT Model



Short Resistance (Ω•m³)

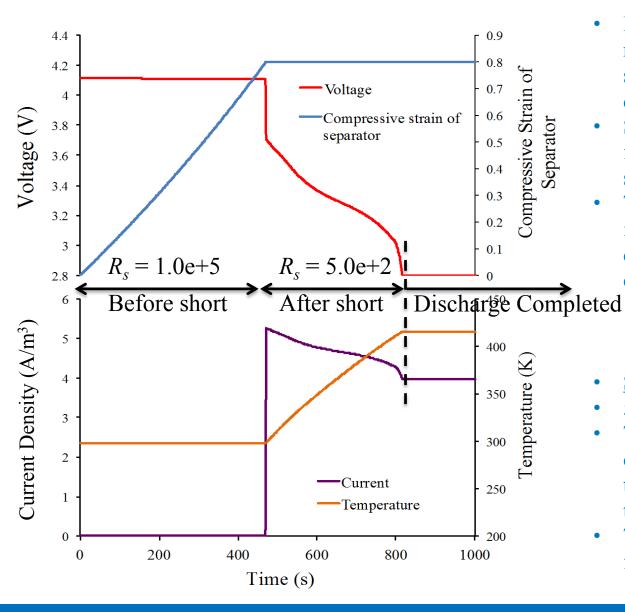
Different type of shorts can be distinguished by the short area for the different failure modes of separator layer, e.g. tensile failure or shear failure.

$$R_{short} = A_{short} \sum \frac{1}{\kappa_s^{(i)}}$$

Temperature

Temperature is assumed to be uniform across each LSDYNA macro element. And the temperature rise is calculated based on the generation of joule heating energy and electrochemical reaction heats.

NREL Single-Element Demonstration of MECT Model

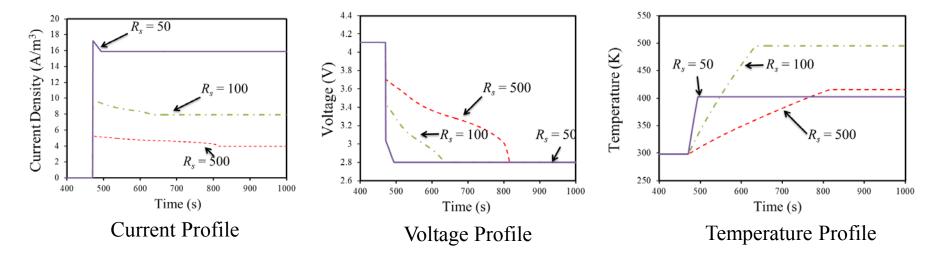


- Linear elastic mechanical response for electrodes and separator were used for demonstration purposes.
- Strain based failure criteria for separator was used to simulate short-circuit.
- The current shows an instant increase and then starts drop due to the decrease in the cell voltage.

- <u>Simulation Conditions:</u>
- 5 Ah LiCoO₂/graphite cell
- The cell voltage of fully discharged is set to 2.8V and the battery model stops after that.
- The model uses 2 minutes for 10⁶ time steps.

NREL Numerical Study on the Effect of Short Resistance

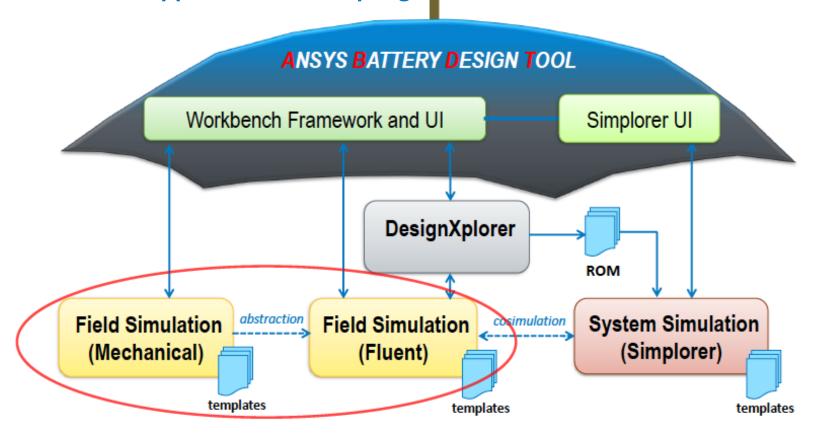
 The developed MECT model is further utilized here to investigate the effect of short resistance on the battery cell performance



- The model captures the effect of short circuit resistance on the subsequent electrical response.
- With the decrease of short circuit resistance, the instantaneous increase of current and voltage drop increases, the discharging completes in a much quicker manner.
- The temperature profile is consistent with the voltage/current evolution profiles, a lower short-circuit resistance does not always produce a higher temperature: there are trade-offs between the cell's energy content, how fast it can be dissipated as heat in the electrochemical models versus heat transfer rates away from the point of generation.

ANSYS Integration of Mechanical - ECT Coupling

 ANSYS implementing the developed MECT model in ANSYS products, providing technical supports on the coupling method



- Convenient "vertical app" around standard ANSYS products
- Plug-and-play with other products via open-standard interfaces











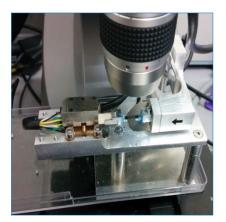


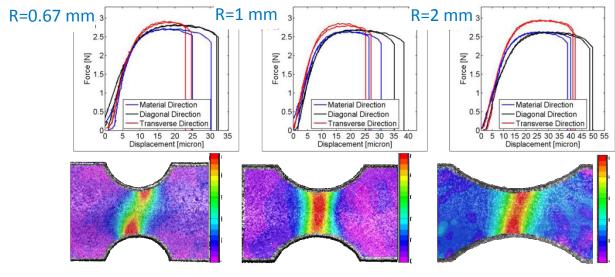


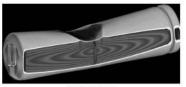
MIT Mechanical Characterization

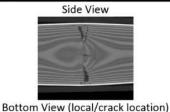
 MIT providing experimental and model inputs, to support the mechanical constitutive and fracture modeling of battery cell components

Micro testing of collectors







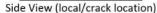




CT images of ← cell fracture









Fracture __ modeling



Top View (Longitudinal Crack)

View of Cross Section









Institute of Technology



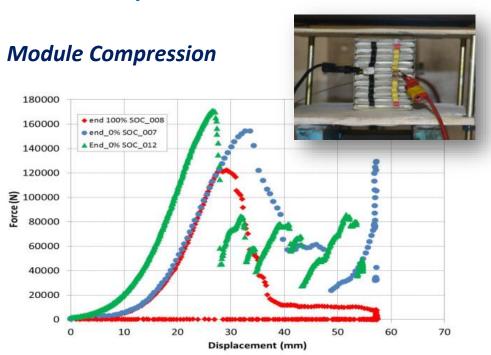


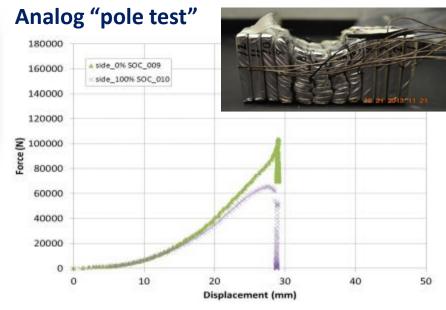




SNL Abuse Testing of Batteries

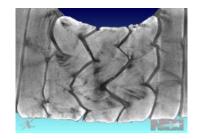
SNL providing experimental of abuse test of batteries to support MECT model development

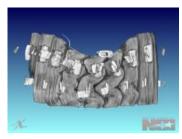




CT image of structural failure

- Determining coupled failure behavior of batteries during crush/impact testing
- Providing module level data support for validation of MECT model















Institute of Technology





SNL Abuse Testing Planned

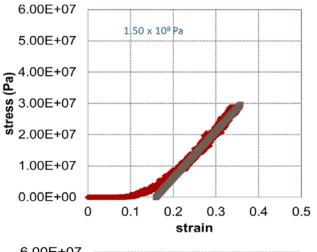
- Single cell end crush new fixture built for single cell tests
- Failure mode investigation Crush and CT analysis of charged and discharged packs crushed to predetermined displacement
- Dynamic Testing drop testing at burn site

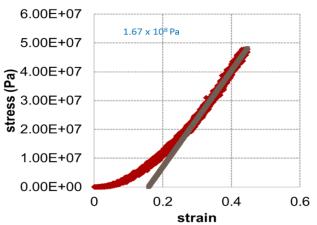






Single cell test data





Future Work – Task 2

- Full cell numerical study using the material model presented in this report.
- Verification compared with existing electrochemical models, for example, ANSYS MSMD model.
- Evolve ABDT into standard Analysis System in Workbench
- Work with MIT on fracture modeling of battery cell components.
- Validation against test data from Sandia.













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Task 3 – Microstructure Modeling

Developing advanced microstructure models as tools to design *3.* battery electrodes through a better understanding of basic physics at the particle and electrode levels. Build upon existing microstructure models. Fabricate and test electrode samples with different characteristics, also obtain tomography images, to build enhanced and validated microstructure models.

> Task 3 PI NREL, **Kandler Smith**

Microstructure Modeling TAMU, Partha

Electrode Fabrication/testing ANL, Daniel





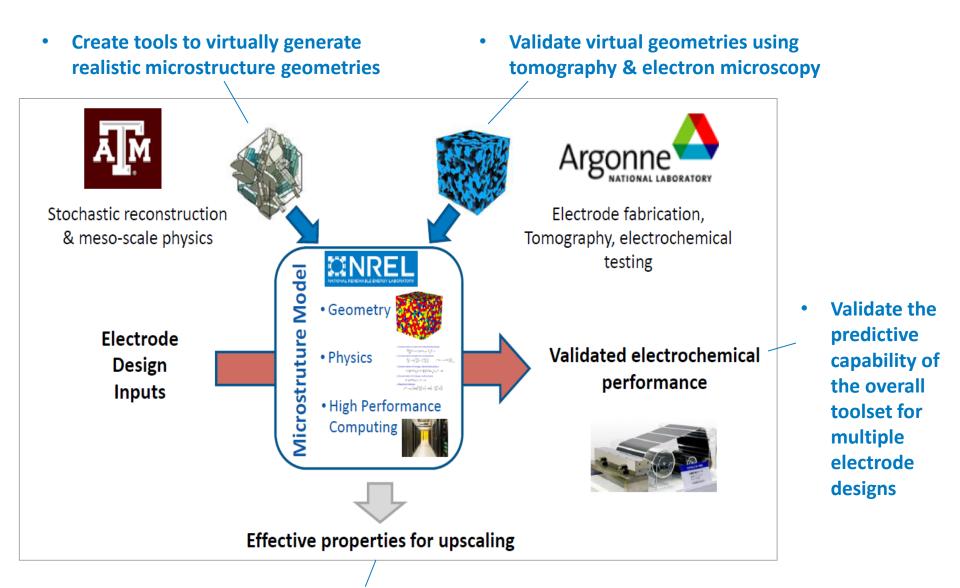








Overview of 3D Microstructure Modeling



Bridge to cell and pack CAE toolsets

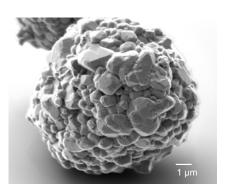
Technical Accomplishments - Microstructure

- Defined electrochemical physics of interest for microstructure modeling
- Demonstrated echem simulations on 2D and 3D geometries
- Developed draft experimental test plan with ANL CAMP, complementing ABR programs
- Received first baseline electrode data
- Developing new methodology to automate tomography reconstruction with TAMU
- Prototyping tools for virtual geometry construction with TAMU

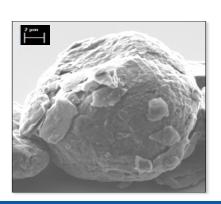
Argonne National Lab Experimental Validation

- ANL providing model inputs (recipe), experimental samples, electrochemical and tomographic measurements
- Initial focus: NMC532/graphite from ABR program
 - Leverage baseline electrochemical datasets already available
- 3 year validation study to include electrode design variants
 - Multiple loading & calendaring conditions for validating microstructure models at several electrode thicknesses & porosities
 - Provides opportunity to explore performance & degradation physics documented from previous ANL-ABR studies and apply knowledge in future design tools

NMC532



Graphite

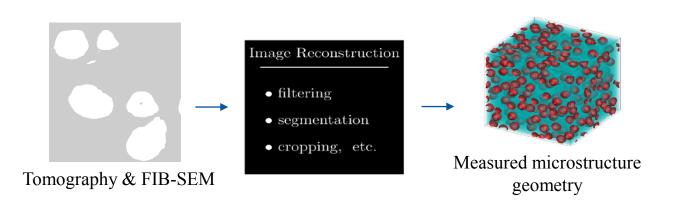


SEM images courtesy of Daniel Abraham & Andy Jansen, ANL CAMP facility

Texas A&M Geometry Stochastic Reconstruction

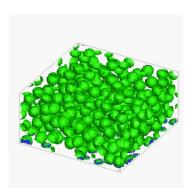
Two paths:

1) Image-based, supporting experimental validation



2) <u>Virtual path</u>, supporting computer-aided design without need for prototype

 \log normal variable (x)



Recipe & material inputs

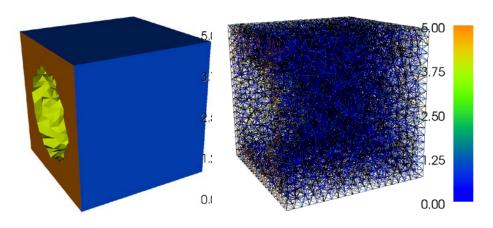
Virtual microstructure geometry

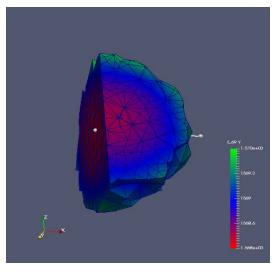
3D simulation Validation

Physics exploration

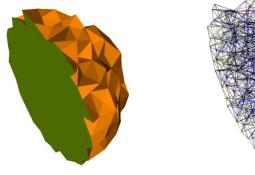
NREL Electrochemical Simulation Tool Development

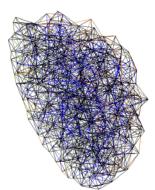
Same code solves both 2D and 3D cases Scalable for high performance computing, 3D domains and meshes



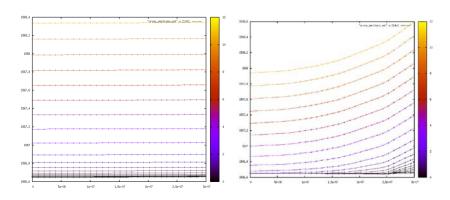


Concentration profile Inside solid particle





(About 11K degrees of freedom. About 10 sec/time step on one core.)



Response to change in solid phase diffusivity

Future Work for Task 3

- Tomographic characterization of baseline electrode geometry
- Electrochemical simulation of baseline electrode microstructure
 - Virtual reconstructed geometry
 - Tomographic reconstructed geometry
- Model enhancements based on baseline electrode model validation study
- Modeling and validation for thick electrode design variants















Responses to Previous Year Reviewers' Comments

New Project in FY16 so not reviewed last AMR.















Collaborators and Partners

Project Leader NREL, Ahmad Pesaran Task 2 PI Task 3 PI Task 1 PI **Industry Advisory** NREL. NREL, **NREL**, Shriram CSWG, Bill Stanko **Kandler Smith** Gi-Heon Kim Santhanagopalan **Other Team Members:** Material Microstructure Cell/Electrode Daniel Abraham, ANL Characterization Modeling Making Partha Mukherjee, TAMU MIT, Elham ANL, Daniel TAMU, Partha Chris Orendorff, SNL Stephen Dajka, ANSYS Electrode **Abuse Testing** Elham Sahraei Esfahani, MIT Fabrication/testing SNL, Josh Chao Zhang, NREL ANL, Daniel Dennis Dees, ANL Mike Sprague, NREL Cell/Module Joshua Lamb, SNL **Fabrication** Chuanbo Yang, NREL ANL, Daniel Andrew Jansen, ANL Genong Li, ANSYS Integration Lei Cao, NREL ANSYS, Stephen Massachusetts















Summary

- Task 1. New GH-MSMD provides 100-1000x computation speed-up in battery electrochemical/thermal simulation
 - Retains modularity of particle, electrode, cell, pack domains
 - Journal article in preparation
 - Speed enables direct full model use in parameter identification
- Task 2. Simultaneously coupled mechanical-electrochemical-thermal model for mechanical abuse simulation
 - Enables simultaneous modeling of electrochemical reactions during the short, when necessary
 - o Studies the interactions between mechanical failure and battery cell performance
 - o Improves the flexibility of the model for various batteries structures and loading conditions
 - Model validation is ongoing to compare with test data from SNL
 - Established ABDT tool in ANSYS
- Task 3. Microstructural modeling to enhance next gen. electrode designs
 - 3 year project to validate models for variety of electrodes complementing Advanced
 Battery Research programs
 - o Prototype tools have been developed for echem simulation and geometric reconstruction















Acknowledgements

- We appreciate support and funding provided by Vehicle Technologies Office at the US Department of Energy
 - Brian Cunningham
 - David Howell

















Technical Back-Up Slides

NREL MECT Model Mechanical Homogenization

- This example uses linear elastic models for illustrative purposes; but the model can easily accommodate user-defined constitutive models for the mechanical response.
- A generic micro-mechanical model for homogenization of the different layers was introduced to improve computational efficiency of the coupling scheme.
- The constitutive equations when reorganized in specific ways enable
 easier interpretation of
 experimentally measurable
 responses such as in-plane and
 through-plane stresses.

Constitutive equations

$$\sigma_{ij} = C_{ijkl} \varepsilon_{kl}$$

Re-organization of matrix components

$$\left\{ \begin{array}{c} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \\ \sigma_{33} \\ \sigma_{23} \\ \sigma_{13} \end{array} \right\} = \left[\begin{array}{c|cccc} C_{11} & C_{12} & C_{16} \\ C_{12} & C_{22} & C_{26} \\ C_{16} & C_{26} & C_{66} \end{array} \right] \left\{ \begin{array}{c} C_{13} & C_{14} & C_{15} \\ C_{23} & C_{24} & C_{25} \\ C_{36} & C_{46} & C_{56} \end{array} \right] \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{12} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{13} \end{array} \right.$$

$$\left\{ \begin{array}{c} \sigma_{13} & C_{23} & C_{26} \\ C_{14} & C_{24} & C_{46} \\ C_{15} & C_{25} & C_{56} \end{array} \right\} \left\{ \begin{array}{c} C_{34} & C_{44} & C_{45} \\ C_{35} & C_{45} & C_{55} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{13} \end{array} \right.$$

$$\left\{ \begin{array}{c} \sigma_{1} \\ \sigma_{2} \\ \sigma_{1} \end{array} \right\} \left\{ \begin{array}{c} \sigma_{1} \\ \sigma_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{13} \end{array} \right\} \left\{ \begin{array}{c} \sigma_{1} \\ \sigma_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{13} \end{array} \right\} \left\{ \begin{array}{c} \sigma_{1} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \sigma_{1} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \sigma_{1} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{12} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{23} \\ \varepsilon_{23} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{33} \\ \varepsilon_{24} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{24} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{24} \\ \varepsilon_{25} \\ \varepsilon_{33} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{33} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{33} \\ \varepsilon_{34} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{33} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{33} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{24} \\ \varepsilon_{25} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{23} \\ \varepsilon_{24} \\ \varepsilon_{25} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{24} \\ \varepsilon_{25} \\ \varepsilon_{25} \\ \varepsilon_{25} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{25} \\ \varepsilon_{25} \\ \varepsilon_{25} \end{array} \right\} \left\{ \begin{array}{c} \varepsilon_{11} \\ \varepsilon_{25} \\ \varepsilon$$

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Zhang, Chao et al. IJES 2015

NREL MECT Model Mechanical Homogenization

Macro-meso mechanical homogenization method

• Given that the thickness of the different layers is several orders of magnitude smaller than the in-plane dimensions, we have the following assumptions for building the effective stress/strain relationships:

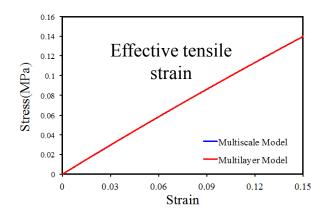
$$\overline{\mathcal{E}}_{=} = \mathcal{E}_{=}^{(1)} = \mathcal{E}_{=}^{(2)} = \dots = \mathcal{E}_{=}^{(N)} \qquad \overline{\sigma}_{\perp} = \sigma_{\perp}^{(1)} = \sigma_{\perp}^{(2)} = \dots = \sigma_{\perp}^{(N)}
\overline{\mathcal{E}}_{\perp} = \upsilon^{(1)} \mathcal{E}_{\perp}^{(1)} + \upsilon^{(2)} \mathcal{E}_{\perp}^{(2)} + \dots + \upsilon^{(N)} \mathcal{E}_{\perp}^{(N)}
\overline{\sigma}_{=} = \upsilon^{(1)} \sigma_{=}^{(1)} + \upsilon^{(2)} \sigma_{=}^{(2)} + \dots + \upsilon^{(N)} \sigma_{=}^{(N)}$$

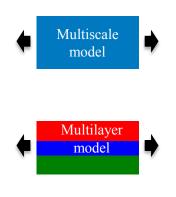
Regrouping the terms as discussed in the previous slide provides explicit expressions
for the effective stiffness of the cell-sandwich, from properties of individual
components (e.g. separator, anode and cathode).

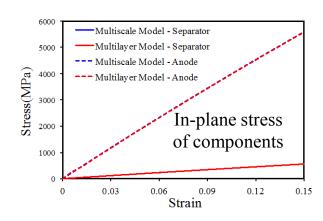
$$\bar{C}_{\perp} = \left[\sum_{i=1}^{N} v^{(i)} (C_{\perp}^{(i)})^{-1} \right]^{-1} \qquad \bar{C}_{\times}^{T} = \left[\sum_{i=1}^{N} v^{(i)} C_{\times}^{(i)^{T}} (C_{\perp}^{(i)})^{-1} \right]^{-1} \bar{C}_{\perp}
\bar{C}_{\times} = \bar{C}_{\perp} \left[\sum_{i=1}^{N} v^{(i)} (C_{\perp}^{(i)})^{-1} C_{\times}^{(i)} \right] \qquad \bar{C}_{=} = \sum_{i=1}^{N} v^{(i)} C_{=} + \sum_{i=1}^{N} v^{(i)} C_{\times}^{(i)^{T}} (C_{\perp}^{(i)})^{-1} (\bar{C}_{\times} - C_{\times}^{(i)}) \right]$$

NREL MECT Model Verification of Mechanical Homogenization

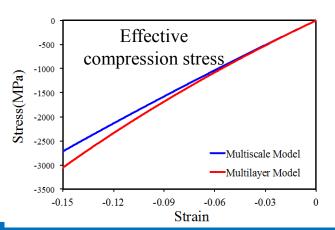
 Numerical comparison of the full-scale multi-layer model against the efficient macro-meso mechanical homegenization models capture the mechanical response under in-plane tension (main failure mode of cell components) accurately.

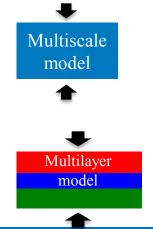


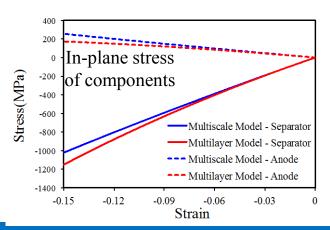




• Other failure modes such as through-thickness compression show the need for more sophisticated mixing rules beyond the linear combination of component properties used in this version.







NREL MECT Model Electrochemical-Thermal Model

Pseudo 2D electrochemical-thermal model

• The battery model uses the same set of equations from our previous CAEBAT efforts, building on the Newman model.

Charge Transfer Kinetics at Reaction Sites

$$j^{Li} = a_s i_o \left\{ \exp \left[\frac{\alpha_a F}{RT} \eta \right] - \exp \left[-\frac{\alpha_c F}{RT} \eta \right] \right\} \qquad i_0 = k(c_e)^{\alpha_a} (c_{s, \max} - c_{s, e})^{\alpha_a} (c_{s, e})^{\alpha_a} (c_{s, e})^{\alpha_b} \qquad \eta = (\phi_s - \phi_e) - U$$

Species Conservation

$$\frac{\partial c_s}{\partial t} = \frac{D_s}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial c_s}{\partial r} \right)$$

$$\frac{\partial (\hat{\varepsilon}_e c_e)}{\partial t} = \nabla \cdot (D_e^{\text{eff}} \nabla c_e) + \frac{1 - t_+^0}{F} j^{Li} - \frac{i_e \cdot \nabla t_+^0}{F}$$

Charge Conservation

$$\nabla \cdot (\hat{\sigma}^{eff} \nabla \phi_{s}) - j^{Li} = 0$$

$$\nabla \cdot \left(\kappa^{eff} \nabla \phi_e \right) + \nabla \cdot \left(\kappa_D^{eff} \nabla \ln c_e \right) + j^{\text{Li}} = 0$$

Energy Conservation

$$\rho c_p \frac{\partial T}{\partial t} = q$$

$$q = j^{Li} \left(\varphi_s - \varphi_e - U + T \frac{\partial U}{\partial T} \right) + \hat{\sigma}^{eff} \nabla \varphi_s \cdot \nabla \varphi_s + \kappa^{eff} \nabla \varphi_e \cdot \nabla \varphi_e + \kappa_D^{eff} \nabla \ln c_e \cdot \nabla \varphi_e$$

Short Current

$$i_{short} = \frac{\phi_{1,p} \left|_{lp} - \phi_{1,n} \right|_{0}}{R_{short}}$$

Appendix

 $d\overline{\varepsilon}$: strain increment

dt: time step

t: time

T: temperature

T': updated temperature

 ε_i : strain of components

 σ_i : stress of components

 $\overline{\varepsilon}$: effective strain

 $\overline{\sigma}$: effective stress

dt': mapped time step for electrochemical model

t: mapped time for electrochemical mod el

 R_{short} : short resis tan ce

 Ks_i : conductivity of cell components